# Dynamic soil property change in response to disturbance from conventional/unconventional gas drilling infrastructure in Pennsylvania Cody M. Fink\*, Patrick J. Drohan

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#### **Introduction**

PENNSTATE

Pennsylvania's landscapes have undergone extensive oil and gas development for over 150 years. The recent discovery and development of unconventional shale-gas reserves suggests extensive additional disturbance across the state is possible. Development of gas drilling infrastructure including well pads, gathering lines, frac ponds, roads, and staging areas has the potential to alter dynamic soil properties (DSP), which are soil properties documented to change with disturbance over time. Soil bulk density (BD) and penetration resistance are DSPs of

#### **Objectives**

 Determine the effect of gas drilling disturbance on soil bulk density
 Compare disturbance effects of conventional vs. unconventional gas infrastructure
 Evaluate the use of

nuclear density gauges

to monitor soil

compaction



interest as indicators of soil compaction after disturbance. The rocky soils often encountered in Pennsylvania's gas region make measuring BD with traditional methods difficult.

### **Materials and Methods**

## **Field Sites**

- Conventional gas infrastructure
- 12 pads with disturbance dating back to at least
  1930
- 5 pads with no disturbance prior to 1980
- Historical aerial photography (PennPilot) used to identify approximate disturbance date (hard to verify)
- Unconventional (hydraulically fractured) shale-gas infrastructure
- 1 pipeline constructed in 2011



pad Temporary restoration Tippeline Tippeline



1930s pad

**1960s pipeline** 



1930s 1980s Surface measurement for 1930s and 1980s pads









**Figures 5a-5d.** DSP data for conventional gas sites (\* indicates significance at alpha=0.05; NF=native forest; D=disturbed) **a.)** Bulk density from core method **b.)** pocket pentrometer **c.)** dynamic cone penetrometer **d.)** dry density from Troxler gauge

#### Unconventional shale-gas site

Dynamic cone penetrometer

700.00

600.00

**Ξ** 500.00

**a** 400.00

.<u>.</u> 300.00

**9** 200.00

100.00

**Figure 1.** Location of research sites in Pennsylvania

Figure 2. Direct transmission (top) and backscatter geometries (bottom) for nuclear density gauge. (Troxler Electronic Laboratories, Inc.)

#### **Data Collection**

Dry density was measured with a Troxler Moisture Density Gauge (Model 3411-B) at three random spots on the disturbed (D) and adjacent undisturbed forest (NF) soils. Readings were taken at the soil surface and 8" depth in backscatter and direct transmission modes, respectively. Dry density is reported as an average of the material between the source rod and the gauge base, including rock fragments and organic material.

Soil bulk density values were obtained using the core method

	Mean Dry [	Mean Dry Density (g/cm <sup>3</sup> )		
	BS	8in		
Disturbed (D)	0.94	1.34		
1930s pads Forest (NF)	0.80	1.06		
p-value	0.040	<0.001		
Disturbed (D)	1.10	1.52		
1980s pads Forest (NF)	0.93	1.21		
p-value	0.125	0.002		

Figure 4. Conventional gas infrastructure

1980s pad

1984 pipeline



2011



**Figures 6a-6b.** DSP data for unconventional shale-gas site (\* indicates significance at alpha=0.05; NF=native forest; P=pipline **a.**) dynamic cone penetrometer **b.**) dry density from Troxler gauge

	Mean Dry Density (g/cm <sup>3</sup> )				
pipeline	BS	2in	4in	6in	8in
line (P)	1.3	1.52	1.65	1.74	1.74
st (NF)	0.9	0.82	0.97	1.1	1.13
lue	0.003	< 0.001	< 0.001	< 0.001	< 0.001

#### **Future Work**

# 1930s1980sDepth intervals (BS=surface; 8=8in) for 1930s and 1980s pads

#### **Conclusions**

- The BD core method proved unreliable on the rocky soils encountered. The nuclear density gauge, while only capable of reporting a depth averaged value, is an effective indicator of compaction and takes less than 5 min. per sample
- The 1930s and 1980s conventional gas sites have significantly higher dry density and penetration resistance on the disturbed compared to the forested soil.
- Dry density on the 2011 gas pipeline was significantly higher than the forested soil.
   Compared to the conventional pads, the pipeline had higher density values, with

(Soil Survey Staff, 2004); a random hand excavated pit on the D and NF soils was described to 40cm and three 2"x2" core samples were taken from the 1<sup>st</sup> and 2<sup>nd</sup> master horizons. Penetration resistance was measured on the D and NF soils at 10 regularly spaced intervals along a 30m transect. A dynamic cone penetrometer was driven to depths of 5cm, 10cm, and 15cm; number of drops with a 2kg slide hammer was converted to total kinetic energy. Surface measurements of unconfined compressive strength were taken with a pocket penetrometer.

Soil Texture	Ideal Bulk densities	that may affect root growth	that restrict root growth
	g/cm3	g/cm3	g/cm3
Sands, loamy sands	<1.60	<1.60 1.69	
Sandy loams, loams	oams, loams <1.40 1.63		1.8
Sandy clay loams,			
loams, clay loams	<1.40	1.6	1.75
Slilt, silt loams	ams <1.30 1.6		1.75
Silt loams, silty clay			
loams	<1.10	1.55	1.65
Sandy clays, silty			
clays, some clay			
loams (35-45% clay)	<1.10	1.49	1.58
Clays (>45% clay)	<1.10	1.39	1.47
Source: Pro	tecting Urban S	oil Quality, USDA-N	VRCS
Figure 7. Pennsylvania	a Stormwater E	Best Management	Practices Manua
BMP 6 7 3. Soil Amen	dment & Restr	ration	

 Measure additional DSPs (carbon, nitrogen, phosphorus, penetration resistance, and soil wetness) on gas disturbance sites
 Develop a model to predict problem soil areas

for shale-gas development

those at 4", 6", and 8" potentially restricting to root growth The differences in BD between the conventional and unconventional sites may be attributed to variances in the size of the operation and type of equipment used. Time may also influence recovery of soil BD; this factor is unclear as the exact disturbance dates of the sites in the study is hard to verify